

# Performance Enhancement in Working of Single Slope Solar Still using Different Modifications

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## Article Info

Article history:

Received 5 January 2015

Received in revised form

12 January 2015

Accepted 20 January 2015

Available online 31 January 2015

## Keywords

Distillation,

Single slope solar still

## Abstract

As the population is increasing, fresh water resources are under heavy pressure. A very small fraction, about 3 percent of the available water resources is available as fresh water. Drinking water shortage is expected to become one of the biggest problems for humanity. Many developing countries like India have given topmost priority to fresh water supply in their rural development plans. Distillation is an universal method by which all types of contaminants at any concentration level can be removed. Solar distillation is a method which is energy independent and energy is available free of cost in form of solar radiation. The categorization of solar stills is on the basis of Passive and Active solar stills, basic difference being in case of active solar stills is that in the later the temperature difference between the evaporative and condensing surfaces are increased by feeding the additional thermal energy from the flat plate collector in to the bottom of solar still. The objective of the work is to fabricate a Single slope solar still and to study the affects of various process parameters on the performance of solar still, economic viability, cost of distillate, energy balance of solar still and comparison of experimental results for solar still on periodic (hourly, daily & monthly) basis.

## 1. Introduction

Fresh water is basic needs of human and without this life will be impossible. About 70 percent of the total water available on earth is fresh water. Out of this, only 1 percent is accessible as surface freshwater while the rest 2 percent is locked away in the form of ice caps and glaciers in the Polar Regions, far distant from human habitation. At the current trend of growth, global population is expected to reach 8 billion by 2025 and the per capita water available will come down. The average amount of fresh water per capita may still be enough to meet human needs, if it is properly distributed. But equitable distribution is not possible due to mainly two reasons. The first is: two-thirds of the global population (around 4 billion) lives in areas receiving only one-fourth of the global annual rainfall and the second is that the rainfall is not uniform throughout the seasons and from year to year. Supply of potable water to all is the biggest challenge before the world today. Limited resources have resulted in water shortage in 88 developing countries across the world containing 50% of the world's population. Further water supply in these countries cannot meet urban and industrial development needs as well as associated changes in lifestyle.

India is a case in point. From a per capita annual average of 5,177 m<sup>3</sup>, fresh water availability in India dropped to 1,820 m<sup>3</sup> in 2001. It is predicted that by 2025, per capita annual average fresh water availability will be approximately 1,340 m<sup>3</sup> (CPCB (2000)). As the demand for water increases so does the cost. Caught between the growing demands for fresh water on one hand, and increasing pollution of water on the other, India is one of the countries in the world facing a severe water crisis.

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## 2. Solar Distillation System

### 2.1 Principle

In a simple solar still, solar radiation passes through the glass cover. This solar energy is almost entirely absorbed by the black cover on the basin while it is partially absorbed in the thin saline water layer. Thus, saline water and basin are heated by the solar energy. The heat is convected from the black surface into the saline water and the temperature of the saline water increases. Vaporization takes place at the interface, saline water surface and air inside of the solar still, at the interface temperature  $t_i$ . Interfacial area, saline water surface is semi permeable. A plane is called semi permeable when the mass flux of one component is zero. Such a plane is, for instance, the surface of water, which evaporates into an adjoining air stream. Thus, at the interface, the saturated air at the temperature,  $t_i$ , is transported by diffusion due to the partial pressure difference and convection due to the natural convection of the humid air from the interface into the air inside of the solar still with the temperature  $t_r$ . In steady state or quasi-steady state conditions, the air inside of the solar still is also saturated at the temperature,  $t_r$ . Therefore, the humid saturated air inside of the solar still will condense at the glass cover, which has a lower temperature,  $t_g$  than the air temperature inside solar still,  $t_r$ . Heat of condensation heats the glass cover. The glass cover exchanges heat with surrounding and air inside the still by convection and radiation. The condensate flows down, collecting along the glass cover and then in a channel at the end of the glass cover on the south side of the still. Finally, it is collected in a storage bottle outside of still. The schematic view of the solar still is shown in Fig. 2.1. In order to calculate the daily produced condensed water and efficiency, energy balance method has been applied by making the following assumptions:

- The whole system is in a quasi-steady state condition.
- Heat loss by radiation from the circumferential area is negligible.
- At the base of the sill, temperatures of the walls equal to the water temperature, and the water temperature is the average of the interface temperature,  $t_i$  and the bottom temperature,  $t_b$
- The wind speed is assumed to be constant during the experiment.

The performance of a solar still is generally expressed as the quantity of water evaporated by unit area of the basin in one day, i.e. cubic meters or liters of water per square meter of the basin area per day. This performance of solar still can be predicted by deploying the energy and mass balance equations on the various components of the still. The whole system is in a quasi-steady state condition and the temperatures are assumed not to change in one hour interval of time. The energy balance equations for the whole still glass cover, saline water interface and black plate at the bottom has also been done.

**2.2 Solar Stills**

Most of distillation systems have been abandoned due to very slow production rate as per documented literature survey, however, research in the area of solar distillation is limited in the following academic organizations namely Central Arid Zone Research Institute (CAZRI), Jodhpur, IIT Delhi, and Sardar Patel Renewable Energy Research Institute (SPRER), Anand (India); RYUKYUS, NAGOYA and CHUO Universities (Japan); UNAM Ciudad Universitaria, Coyoacaan (Mexico); ALEXANDRIA University (Egypt); BEN-GURION University of the Negev (Israel); TECHNISCHE Universitat Bergakademie Freiberg (Germany); Jordan University of Science and Technology, Irbid (Jordan); University of Ouargla (Algeria); XiAn Jiao Tong University (China); University of Foggia (Italy); National Centre for Scientific Research (NCSR) "DEMOKRITOS" Laboratory for Solar and other Energy Systems (Greece) .

**2.3 Methodology**

Solar distillation is one of the available methods for water distillation and sunlight is one of several forms of heat energy that can be used to power that process. The idea behind a solar still is very simple: saline water inside a black painted basin enclosed in a completely air tight area formed by a transparent cover is heated up and evaporated due to incident solar irradiance that passes though the transparent cover. Consequently water vapour is directed upward and condenses in pure water as it comes in contact with the cooler inside surface of the cover. The energy that the water absorbs contributes to the temperature rise of the water, which leads to evaporation. Evaporation is a process that occurs when the water molecules on the surface of the water obtain enough kinetic energy to change from the liquid to vapour state. The evaporated molecules add to the water vapour between the glass and the water and create a large temperature difference. This difference in temperature affects the temperature of the water vapour that is inside the still between the glass and the water, which creates natural convection.

A higher temperature difference encourages more convection. The warm water vapour will tend to rise towards the cooler glass cover. When the water vapour

comes in contact with the glass, it will condense because the water molecules will lose the kinetic energy needed to be in the vapour state. Since the glass is angled, gravity will cause the condensed water to flow down towards the collection trough.

Despite the advantage of solar stills, their most important drawback is low water productivity or performance in comparison with other thermal desalination methods and to high land requirement. This happens since productivity rate of solar stills depends on the available solar radiation. For this, research activities nowadays move in the direction towards increasing performance and output of solar stills by using several techniques. These are all targeted on the concept of increasing the difference between saline water temperature and glass cover temperature. The view of the solar still and its technical specifications can be seen in Table 2.1 respectively.

**Table: 1.** Technical Specifications of Single Slope Taper Solar Still

Length	6ft
Width	3ft
Cover inclination	15 °
Glass cover area	1.65m <sup>2</sup>
Absorber plate area	1.59 m <sup>2</sup>
Glass Thickness	5mm
Water depth	2cm



**Fig: 1.** View of Single Slope Solar Still

For calculation of Flux  $I_T$  on tilted surface at any instant

$$I_T = I_b r_b + I_d r_d + I_g r_r \tag{1}$$

Where

$$r_b = \frac{\sin \delta . \sin (\phi - \beta) + \cos \delta . \cos \omega . \cos (\phi - \beta)}{\sin \phi . \sin \delta + \cos \phi . \cos \delta . \cos \omega} \tag{2}$$

For the tilted surface facing due south ( $\gamma = 0$ )

$$r_d = \frac{1 + \cos \beta}{2} \tag{3}$$

And

$$r_r = \frac{\rho(1 - \cos \beta)}{2} \tag{4}$$

$\delta$  In degrees is given by the following relation

$$\delta = 23.45 \sin \left[ \frac{360(284 + n')}{365} \right] \tag{5}$$

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For calculation of  $I_g$

Taking  $I_{sc} = 1.367 \text{ kW/m}^2$

$$H_o = \frac{24 \times I_{sc} \times 3600}{\Pi} \left[ 1 + 0.033 \cos \frac{360n'}{365} \right] \quad (6)$$

$$(\omega_s \sin \phi \cdot \sin \delta + \cos \phi \cdot \cos \delta \cdot \sin \omega_s)$$

[in  $\text{kJ/m}^2\text{-day}$ ]

$$\therefore \frac{\overline{H_g}}{H_o} = \left[ a + b \left( \frac{S}{S_{\max}} \right) \right] \quad (7)$$

$$S_{\max} = \frac{2}{15} \omega_s \quad (8)$$

$$\omega_s = \cos^{-1} \{ \tan(\phi - \beta) \cdot \tan \delta \} \quad (9)$$

$\omega_s$  = Sunrise hour angle

Constants a and b in equation are taken from weather data given by Modi and Sukhatme (1979).

We have assumed that the values of a = 0.25 and b = 0.57 for New Delhi are valid for Moradabad.

$$\frac{\overline{H_d}}{H_g} = 1.411 - 1.696 \left[ \frac{\overline{H_g}}{H_o} \right] \quad (10)$$

The hourly extraterrestrial radiation on a horizontal surface ( $I_o$ ) is obtained by calculating the instantaneous value at the mid point of time intervals and multiplying by 3600 s i.e

$$I_o = I_{sc} \times 3600 \left[ 1 + 0.033 \cos \frac{360n'}{365} \right] (\sin \phi \cdot \sin \delta + \cos \phi \cdot \cos \delta \cdot \cos \omega)$$

[ $\text{kJ/m}^2\text{-h}$ ] (2.11)

The relationship for diurnal variation of the monthly average hourly global radiation at a location is given by

$$\frac{\overline{I_g}}{H_g} = \frac{\overline{I_o}}{H_o} (a_1 + b_1 \cos \omega) \quad (12)$$

Where

$$\left\{ \begin{aligned} a_1 &= 0.409 + 0.5016 \sin(\omega_s - 60^\circ) \\ b_1 &= .6609 - .4767 \sin(\omega_s - 60^\circ) \end{aligned} \right\} \quad (13)$$

For estimating the monthly average hourly diffuse radiation

$$\frac{\overline{I_d}}{H_d} = \frac{\overline{I_o}}{H_o} \quad (14)$$

$$\therefore I_b = I_g - I_d \quad (15)$$

**Table: 2.** Calculation of Efficiency of Solar Still Taking Sample Set Of Data (Without Insulation)

Date: 10<sup>th</sup> June 2014

Time in	Product	Atm .	Temperature ( $^{\circ}\text{C}$ )	$\eta_i$
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hours	from still $m_w$ [kg/hr]	temp $p$ ( $^{\circ}\text{C}$ ) ( $t_a$ )	Moist air temperature ( $t_r$ )	Glas s Surface temperature ( $t_g$ )	Water level interface temperature ( $t_i$ )	Bottom temperature ( $t_b$ )	
12-13	0.51	37	50	48	52	59	25.72

**Calculations**

Latitude  $\phi = 28.58$

No of days  $n' = 161$

$$\text{Declination } \delta = 23.45 \sin \left[ \frac{360(284 + 161')}{365} \right]$$

$$\delta = 23.011^\circ$$

Slope of the glass to the horizontal is taken as  $15^\circ$

$$\omega_s = \cos^{-1} \{ -\tan(\phi - \beta) \cdot \tan \delta \}$$

$$\omega_s = \cos^{-1} \{ -\tan(28.58 - 15) \cdot \tan -23.011 \}$$

$$\omega_s = 95.871^\circ$$

$$\omega_s = 1.672$$

$$S_{\max} = \frac{2}{15} \omega_s = 2/15 \times 95.871$$

$$S_{\max} = 12.78 \text{ hours.}$$

let  $S = 7$  hours.

Now

$$H_o = \frac{24 \times I_{sc} \times 3600}{\Pi} \left[ 1 + 0.033 \cos \frac{360n'}{365} \right] (\omega_s \sin \phi \cdot \sin \delta + \cos \phi \cdot \cos \delta \cdot \sin \omega_s)$$

$$= \frac{24 \times 1.367 \times 3600}{\Pi} \left[ 1 + 0.033 \cos \frac{360 \times 161}{365} \right]$$

$$(1.672 \times \sin 28.58 \cdot \sin(23.011) + \cos 28.58 \cdot \cos(23.011) \cdot \sin 95.871)$$

$$H_o = 40639.76 \text{ kJ/m}^2\text{-hr}$$

$$\text{Or } H_o = 11.28 \text{ kW/m}^2\text{-hr}$$

$$\frac{H_g}{H_o} = \left[ a + b \left( \frac{S}{S_{\max}} \right) \right]$$

Where a = 0.25, b = 0.57

$$H_g = \frac{8.915 \times (0.25 + 0.57) \times 10}{12}$$

$$H_g = 0.454 \text{ KW/m}^2 \text{ hr}$$

$$\frac{H_d}{H_g} = 1.411 - 1.696 \left[ \frac{H_g}{H_o} \right]$$

$$= 1.411 - 1.696 \left[ \frac{6.36}{11.28} \right]$$

$$H_d = 2.892 \text{ kW/m}^2\text{-hr}$$

$$r_d = \frac{1 + \cos \beta}{2}$$

$$= 0.98$$

$$r_r = \frac{\rho(1 - \cos \beta)}{2}$$

Taking  $\rho = .2$

$$r_r = 0.017$$

For 12:00 to 13:00 hours.

$$\omega = 15(12\text{-time in hours})$$

$$\omega = 15(12-12.5)$$

$$\omega = -7.5^\circ$$

$$I_o = I_{sc} \times 3600 \left[ 1 + 0.033 \cos \frac{360n'}{365} \right] \text{ [kJ/m}^2\text{-h]}$$

$$\left( \sin \phi . \sin \delta + \cos \phi . \cos \delta . \cos \omega \right)$$

$$I_o = 1.367 \times 3600 \left[ 1 + 0.033 \cos \frac{360 \times 161}{365} \right]$$

$$\left( \sin 28.58 . \sin(23.011) + \cos 28.58 . \cos(23.011) . \cos(-7.5) \right)$$

$$= 4663.18 \text{ kJ/m}^2\text{-hr}$$

$$= 1.295 \text{ kW/m}^2\text{-hr}$$

For Global hourly radiation:-

$$\frac{I_g}{H_g} = \frac{I_o}{H_o} (a_1 + b_1 \cos \omega)$$

Where

$$\{ a_1 = 0.409 + 0.5016 \sin(\omega_s - 60^\circ) \}$$

$$\{ b_1 = .6609 - .4767 \sin(\omega_s - 60^\circ) \}$$

By substituting  $\omega_s = 95.871$  in above equations we get

$$a = 0.702 \text{ and } b_1 = 0.3815$$

$$I_g / 6.34 = 1.295 / 11.28 (.702 + .381 . \cos -7.5)$$

$$I_g = 0.785 \text{ kW/m}^2\text{-hr}$$

Now For hourly diffuse radiation

$$\frac{I_d}{H_d} = \frac{I_o}{H_o}$$

$$I_d = 1.295 \times 2.892 / 11.28$$

$$I_d = 0.332 \text{ kW/m}^2\text{-hr}$$

$$r_b = \frac{\sin \delta . \sin(\phi - \beta) + \cos \delta . \cos \omega . \cos(\phi - \beta)}{\sin \phi . \sin \delta + \cos \phi . \cos \delta . \cos \omega}$$

$$r_b = \frac{\sin(23.011) \sin(28.58 - 15) + \cos(23.011) . \cos(-7.5) . \cos(28.58 - 15)}{\sin 28.58 . \sin(23.011) + \cos 28.58 . \cos(23.011) . \cos(-7.5)}$$

$$= 0.990$$

$$r_b = 0.990$$

$$I_b = I_g - I_d$$

$$I_b = 0.785 - 0.332 = 0.453 \text{ kW/m}^2\text{-hr}$$

So, total radiation on tilted surface

$$I_t = I_b . r_b + I_d . r_d + I_g . r_r$$

We get

$$I_t = 0.453 \times 0.990 + 0.332 \times 0.98 + 0.785 \times 0.017$$

$$I_t = 0.790 \text{ kW/m}^2\text{-hr}$$

$$\eta_a = \frac{0.51 \times 2368}{3600 \times 0.790 \times 1.65} \times 100$$

$$= 25.72 \%$$

### 3. Distillate Produced on Hourly Basis with Insulation

**Table: 3.** Calculation of Efficiency of Solar Still Taking Sample Set Of Data (With Insulation)

Date: 20<sup>th</sup> June 2014

Time in hours	Product from still m <sub>w</sub> [kg/hr]	Atm . tem p (°C) (t <sub>a</sub> )	Temperature (°C)				η <sub>i</sub>
			Moist air temp (t <sub>i</sub> )	Glass Surface temperature (t <sub>g</sub> )	Water level interface temperature (t <sub>j</sub> )	Bottom temp (t <sub>b</sub> )	
12-13	0.67	38	50	49	52	58	33.72

#### Calculations

$$\text{Latitude } \phi = 28.58$$

$$\text{No of days } n' = 171$$

$$\text{Declination } \delta = 23.45 \sin \left[ \frac{360(284 + 171)}{365} \right]$$

$$\delta = 23.440$$

Slope of the glass to the horizontal is taken as 15°

$$\omega_s = \cos^{-1} \left\{ -\tan(\phi - \beta) . \tan \delta \right\}$$

$$\omega_s = \cos^{-1} \left\{ -\tan(28.58 - 15) . \tan 23.44 \right\}$$

$$\omega_s = 95.98^\circ$$

$$\omega_s = 1.674 \text{ radian}$$

$$S_{\max} = \frac{2}{15} \omega_s$$

$$= 2/15 \times 95.98$$

$$S_{\max} = 12.797 \text{ hours.}$$

Let S = 7 hours.

Now

$$H_o = \frac{24 \times I_{sc} \times 3600}{\Pi} \left[ 1 + 0.033 \cos \frac{360n'}{365} \right]$$

$$\left( \omega_s \sin \phi . \sin \delta + \cos \phi . \cos \delta . \sin \omega_s \right)$$

$$= \frac{24 \times 1.367 \times 3600}{\Pi} \left[ 1 + 0.033 \cos \frac{360 \times 171}{365} \right]$$

$$(1.674 \times \sin 28.58 \cdot \sin(23.44) + \cos 28.58 \cdot \cos(23.44) \cdot \sin 95.98)$$

$$H_o = 40654.50 \text{ kJ/m}^2\text{-hr}$$

$$\text{Or } H_o = 11.299 \text{ kW/m}^2\text{-hr}$$

$$\frac{H_g}{H_o} = \left[ a + b \left( \frac{S}{S_{\max}} \right) \right]$$

Where a = 0.25, b = 0.57

$$Hg = \frac{11.299 \times (0.25 + 0.57) \times 10}{12}$$

$$Hg = 6.349 \text{ kW/m}^2 \text{ hr}$$

$$\frac{H_d}{H_g} = 1.411 - 1.696 \left[ \frac{H_g}{H_o} \right]$$

$$= 1.411 - 1.696 \left[ \frac{6.349}{11.299} \right]$$

$$H_d = 2.896 \text{ kW/m}^2 \text{ -hr}$$

$$r_d = \frac{1 + \cos \beta}{2}$$

$$r_d = 0.98$$

$$r_r = \frac{\rho(1 - \cos \beta)}{2}$$

Taking  $\rho = .2$

$$r_r = 0.017$$

For 12:00 to 13:00 hours.

$$\omega = 15(12 - \text{time in hours})$$

$$\omega = 15(12 - 12.5)$$

$$\omega = -7.5^\circ$$

$$I_o = I_{sc} \times 3600 \left[ 1 + 0.033 \cos \frac{360n'}{365} \right] \text{ [kJ/m}^2\text{-h]}$$

$$(\sin \phi \cdot \sin \delta + \cos \phi \cdot \cos \delta \cdot \cos \omega)$$

$$I_o = 1.367 \times 3600 \left[ 1 + 0.033 \cos \frac{360 \times 171}{365} \right]$$

$$(\sin 28.58 \cdot \sin(23.44) + \cos 28.58 \cdot \cos(23.44) \cdot \cos(-7.5))$$

$$I_o = 4700.58 \text{ kJ/m}^2\text{-hr}$$

$$= 1.305 \text{ kW/m}^2\text{-hr}$$

For Global hourly radiation:-

$$\frac{I_g}{H_g} = \frac{I_o}{H_o} (a_1 + b_1 \cos \omega)$$

Where

$$\{a_1 = 0.409 + 0.5016 \sin(\omega_s - 60^\circ)\}$$

$$\{b_1 = .6609 - .4767 \sin(\omega_s - 60^\circ)\}$$

By substituting  $\omega_s = 90.58$  in above equations we get

a = .703 and b1 = 0.380

$$\frac{I_d}{H_d} = \frac{I_o}{H_o} \quad I_g / 6.49 = 1.172 / 8.919 (.662 + .42 \cdot \cos -7.5)$$

$$I_g = 0.791 \text{ kW/m}^2\text{-hr}$$

Now For hourly diffuse radiation

$$r_b = \frac{\sin \delta \cdot \sin(\phi - \beta) + \cos \delta \cdot \cos \omega \cdot \cos(\phi - \beta)}{\sin \phi \cdot \sin \delta + \cos \phi \cdot \cos \delta \cdot \cos \omega}$$

$$I_d = 1.35 \times 2.896 / 11.299$$

$$I_d = 0.334 \text{ kW/m}^2\text{-hr}$$

$$r_b = \frac{\sin(23.44) \sin(28.58 - 15) + \cos(23.44) \cdot \cos(-7.5) \cdot \cos(28.58 - 15)}{\sin 28.58 \cdot \sin(23.44) + \cos 28.58 \cdot \cos(23.44) \cdot \cos(-7.5)}$$

$$= 0.987$$

$$r_b = 0.987$$

$$I_b = I_g - I_d$$

$$I_b = 0.791 - 0.033 = 0.457 \text{ kW/m}^2\text{-hr}$$

So, total radiation on tilted surface

$$I_g \cdot r_r$$

$$I_t = I_b \cdot r_b + I_d \cdot r_d + I_g \cdot r_r$$

We get

$$I_t = 0.457 \times 0.987 + 0.334 \times 0.98 + 0.791 \times 0.017$$

$$I_t = 0.791 \text{ kW/m}^2\text{-hr}$$

$$\eta_a = \frac{0.67 \times 2368}{3600 \times 0.791 \times 1.65} \times 100$$

$$= 33.73\%$$

#### 4. Results and Discussion

**Table 4.** Hourly Temperatures and Distillate Produced Without Insulation

Date: 10<sup>th</sup> June 2014

Time in hours	Product from still	Atm. temp	Temperature (°C)	$\eta_i$
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	$m_w$ [kg/hr]	(°C) ( $t_a$ )	Moist air temperatur e( $t_r$ )	Glass Surface temperature ( $t_g$ )	Water level interface temperature( $t_i$ )	Bottom temperature ( $t_b$ )	
9-10	0.14	25	49	48	49	51	9
10-11	0.34	29	50	46	51	55	10.21
11-12	0.50	35	52	49	53	60	20
12-13	0.51	37	50	48	52	59	25.72
13-14	0.44	35	49	42	53	55	30
14-15	0.32	32	42	36	50	51	32
15-16	0.10	31	40	32	48	49	35

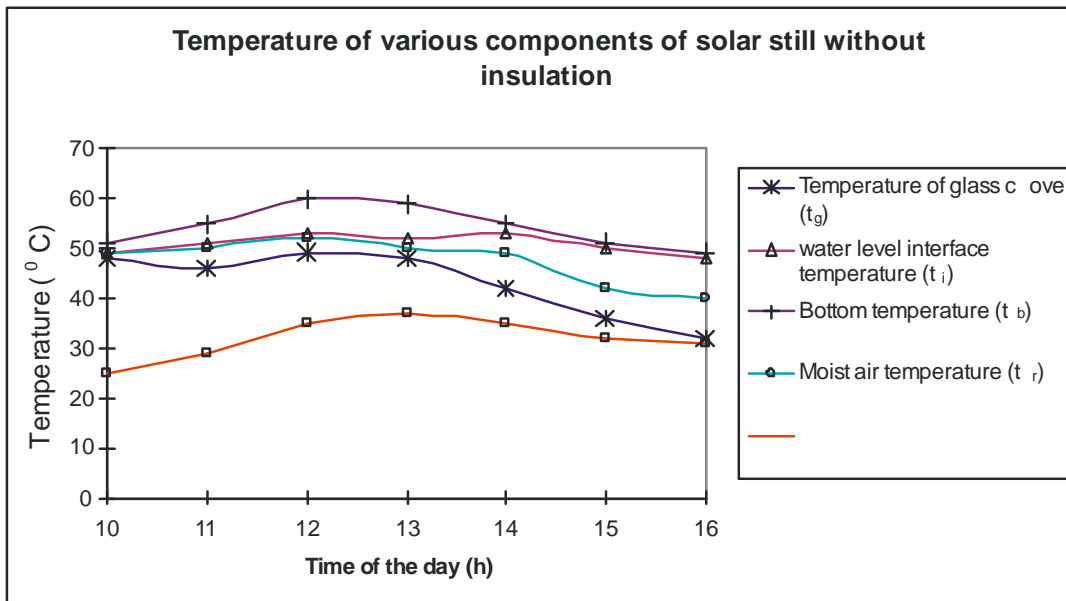
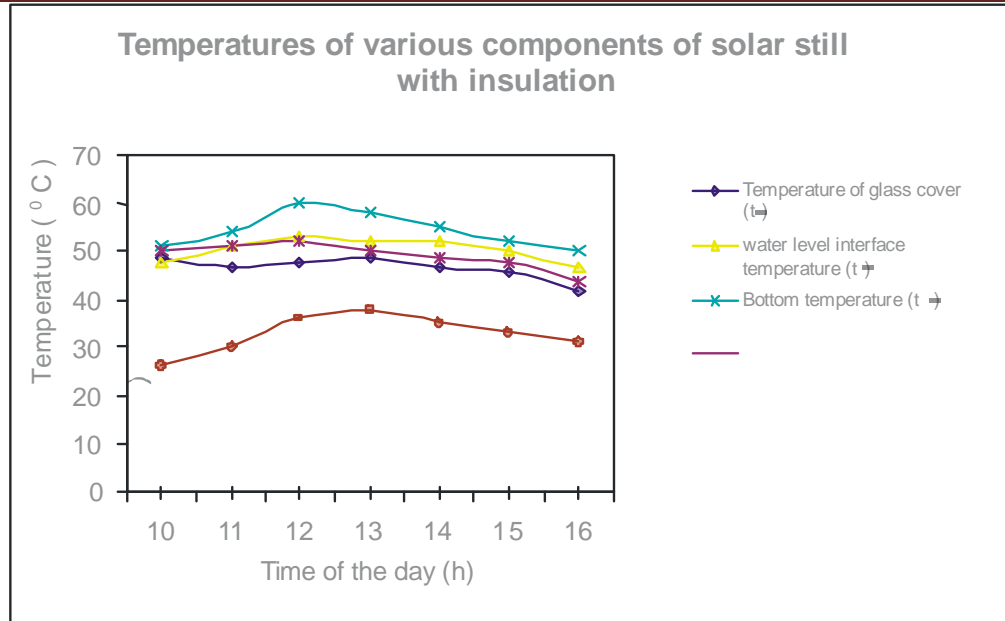


Fig. 2. Temperature of Various Components of Solar Still Without Insulation

Table: 5. Hourly Temperatures and Distillate Produced with Insulation

Date: 20<sup>th</sup> June 2014

Time in hours	Product from still $m_w$ [kg/hr]	Atm. temp (°C) ( $t_a$ )	Temperature (°C)				$\eta_i$
			Moist air temp( $t_r$ )	Glass Surface temperature ( $t_g$ )	Water level interface temperature ( $t_i$ )	Bottom temp( $t_b$ )	
9-10	0.14	26	50	49	48	51	15
10-11	0.40	30	51	47	51	54	17
11-12	0.52	36	52	48	53	60	30
12-13	0.67	38	50	49	52	58	33.72
13-14	0.46	35	49	37	52	55	38.5
14-15	0.36	33	41	36	50	52	41
15-16	0.15	31	40	32	47	50	42.5



**Fig. 3.** Temperature of Various Components of Solar Still with Insulation

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